



# Mapping and Correcting the Wavefront of GQuEST End Mirrors

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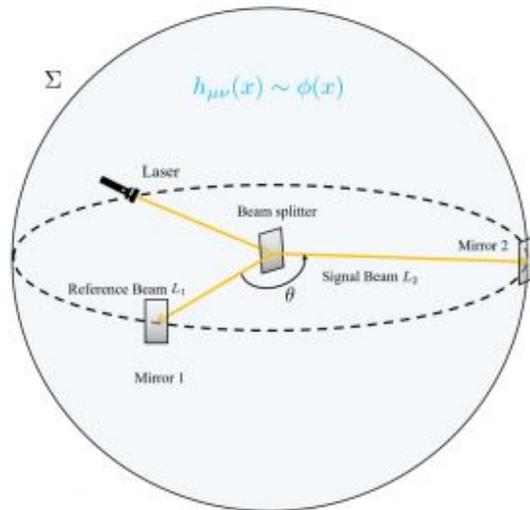
DCC: LIGO-G2401688

# Agenda

- What is GQuEST?
- Mirrors and modes
- Motivation
- Methods
- Wavefront measurement
- Results
  - Simulation
  - Shack-Hartmann
  - Fizeau Interferometer
- What's next?



# Gravity from the Quantum Entanglement of SpaceTime (GQuEST)



*Sphere over which fluctuations can be measured*

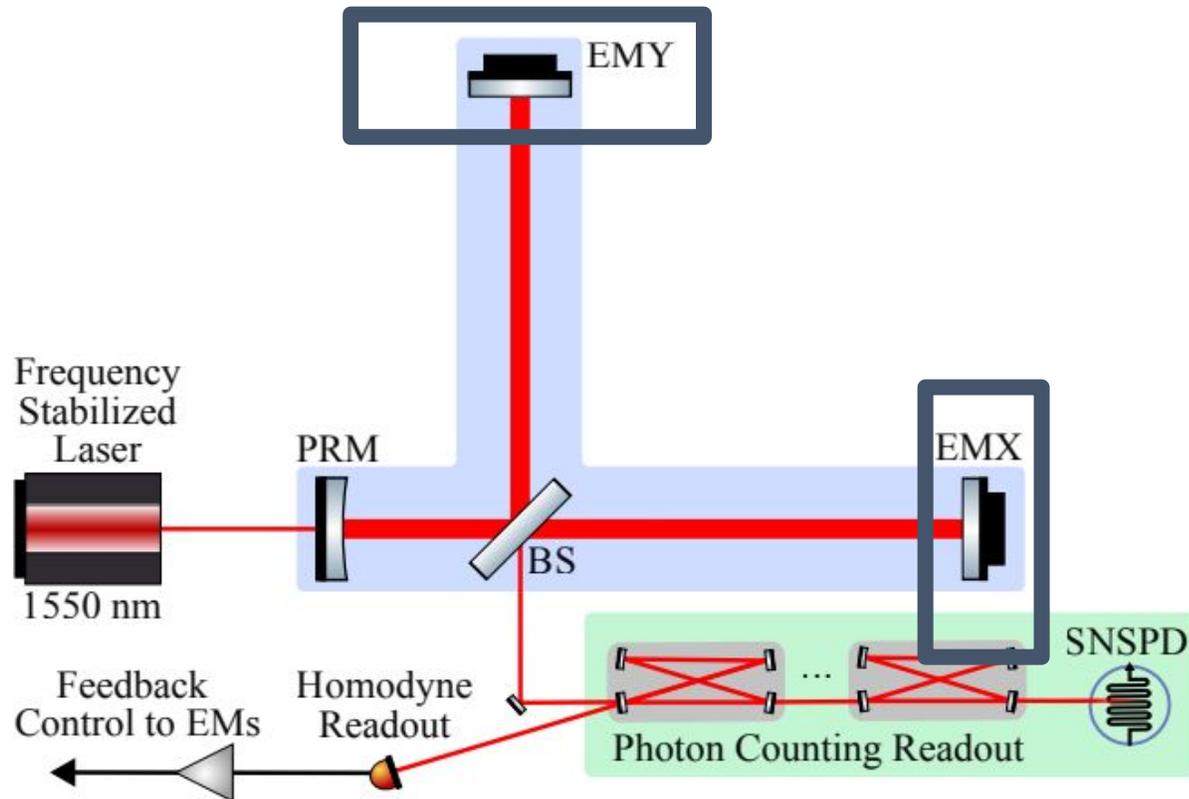
Goal: Sensitivity beyond the standard quantum limit by counting individual photons to measure extremely small fluctuations in space to test proposed theories of quantum gravity.

arXiv:2404.07524

# GQuEST



## Simplified GQuEST Setup



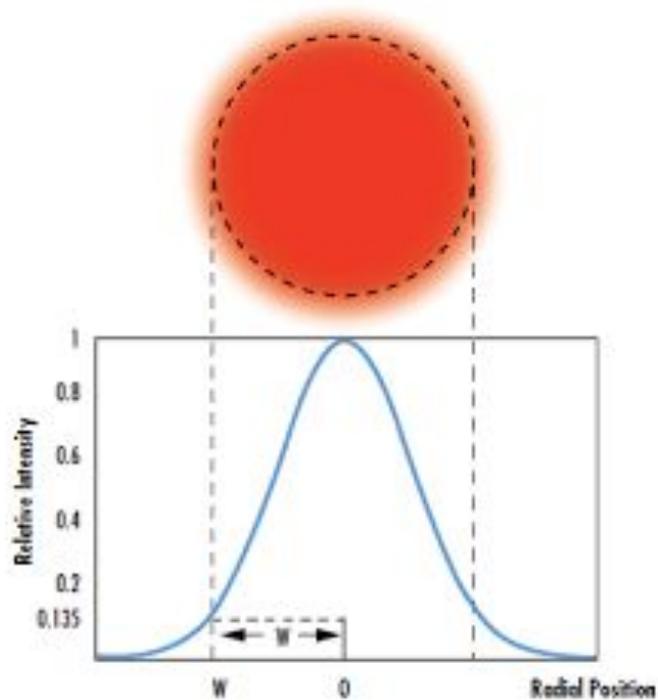
*Vacuum chamber used to hold mirror*

arXiv:2404.07524

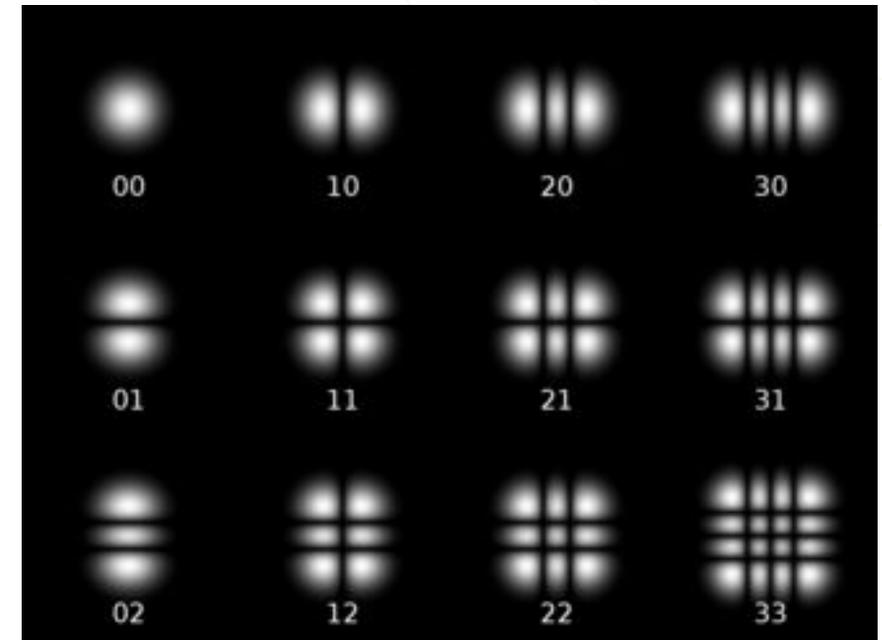
# Mirrors and Modes



*Gaussian beam*

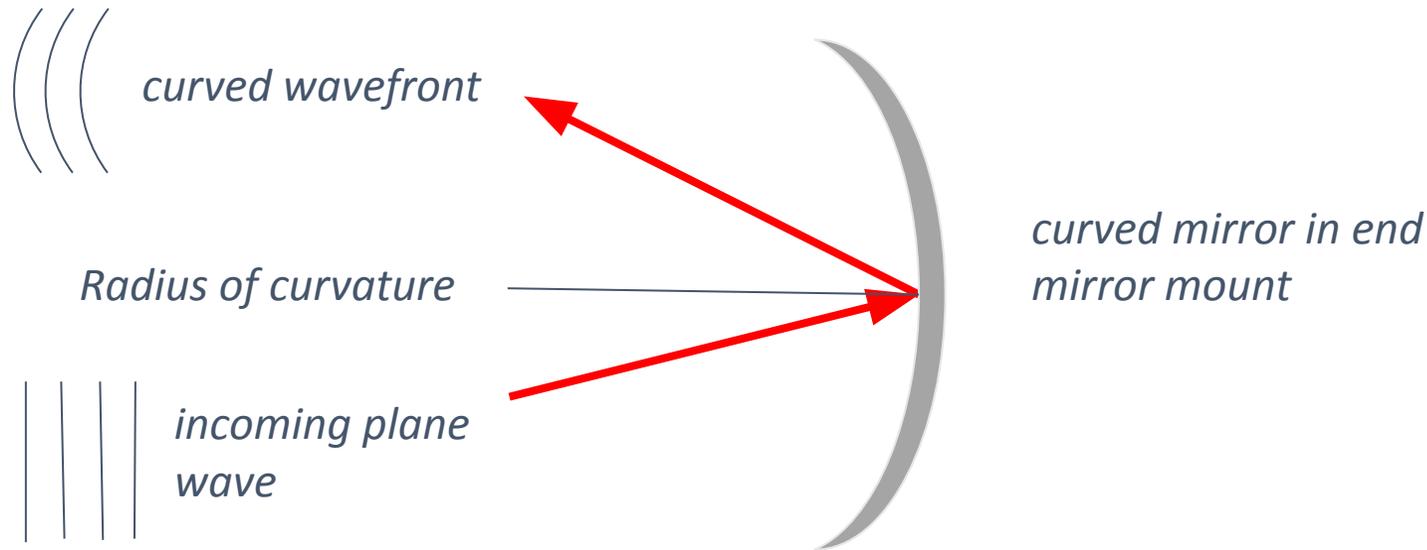


*12 Hermite Gauss modes*



*Hermite-Gauss beams: orthogonal family of laser modes*

# Radius and Coupling

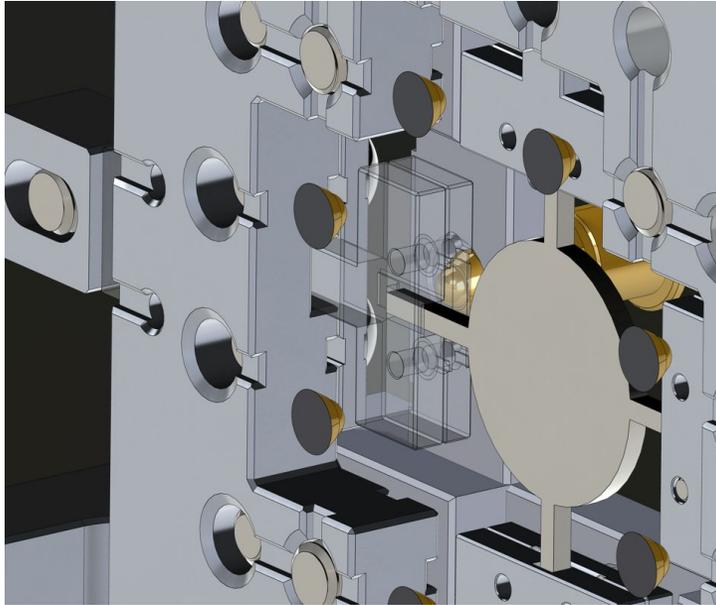


Coupling Coefficient:

How much of our incoming wave is contained in our outgoing wave?

$$k_{mnm'n'}(x, y) = \int \underbrace{HG_{n'm'}^*(x, y)}_{\text{Outgoing Gaussian}} \exp [ik\phi] \underbrace{HG_{nm}(x, y)}_{\text{Incoming Gaussian}} dx dy$$

# Lensing into a mode



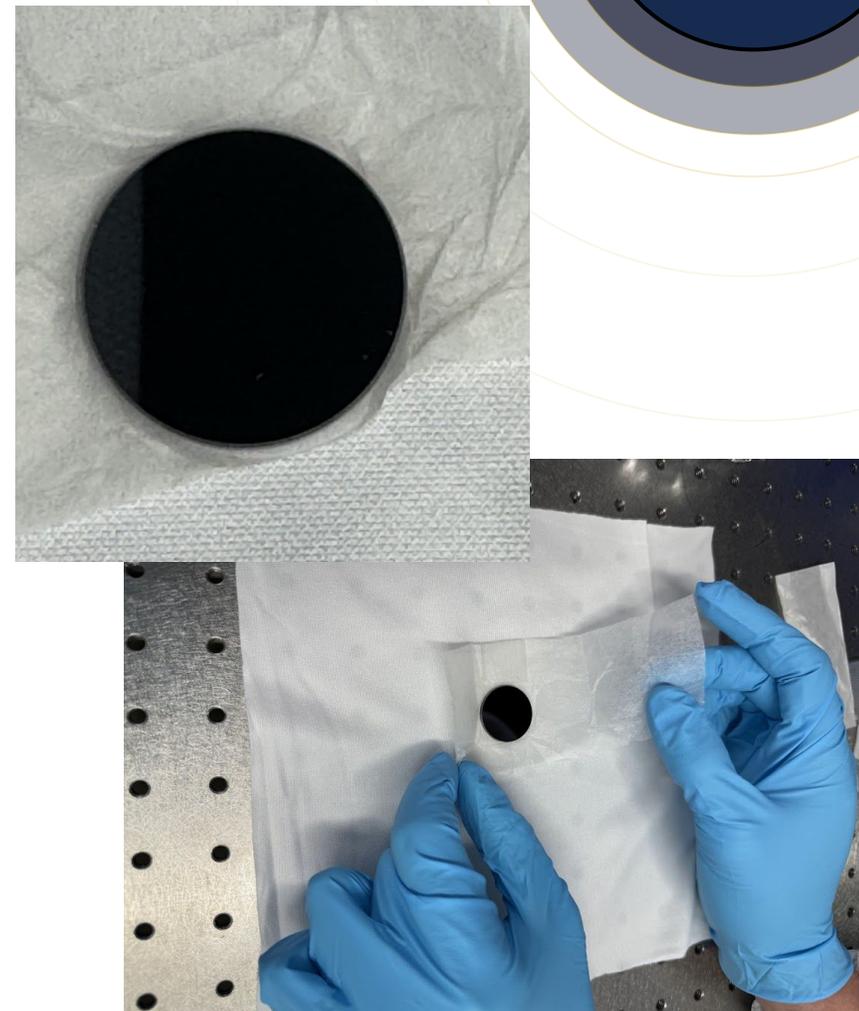
*Design of deformable end mirror*

- Two mirrors in the interferometer need their **modes** to match
- When they do not match, higher order modes create **contrast defects** (extra light in the interferometer)
- Curving the mirror ‘**lenses**’ the mirror into a mode we choose, and we can describe how much by coupling coefficients

# Motivation

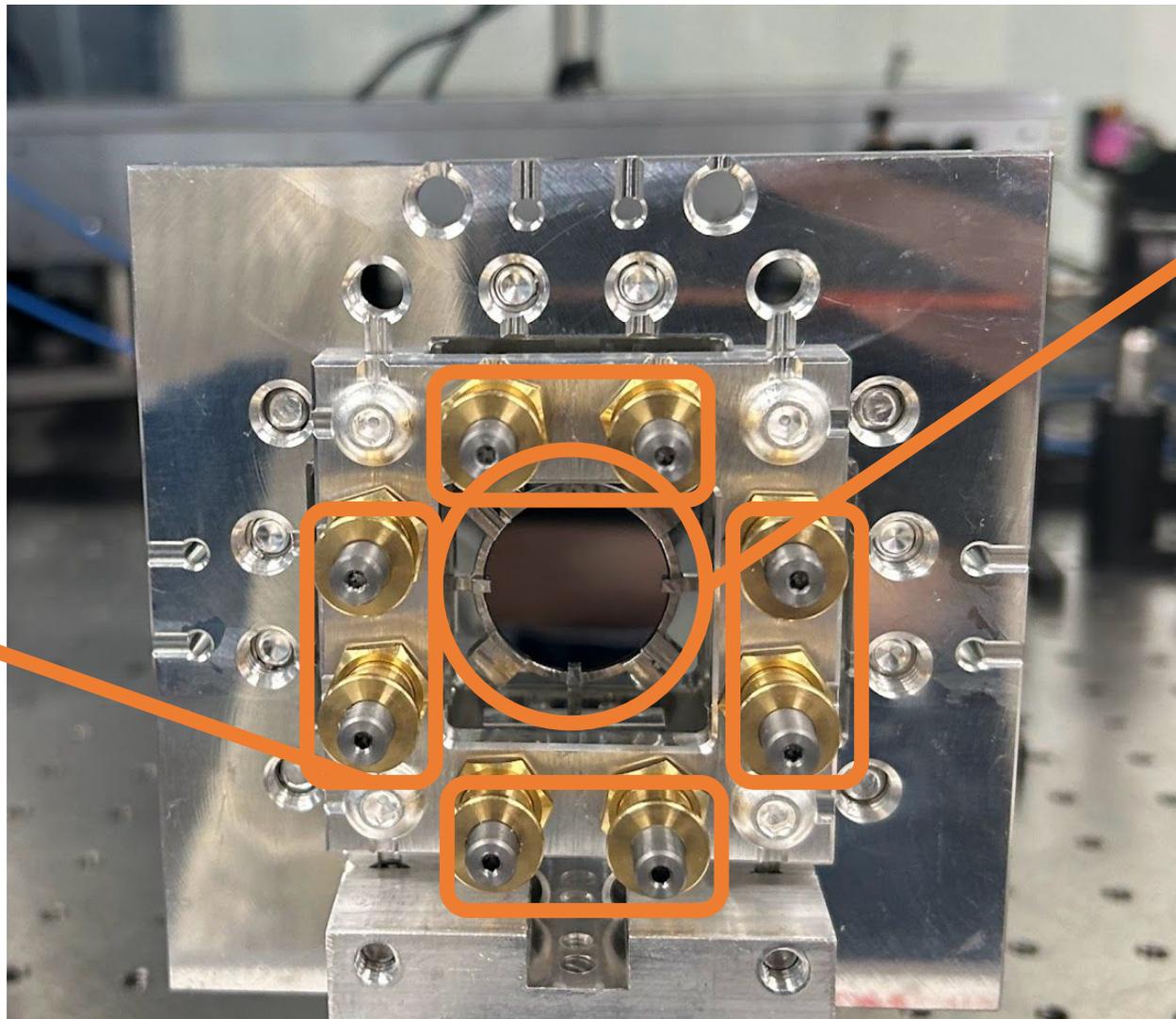
- GQuEST requires very thin mirrors to reduce mechanical noise
- These mirrors will be coated for high reflectivity, which adds stress
- Stress changes the curvature of the mirror
- Curvature changes modes of outgoing light
- **If the modes of the two mirrors do not match, we add contrast defects**
- Contrast defects affect measurement

This means we need wavefront correction!



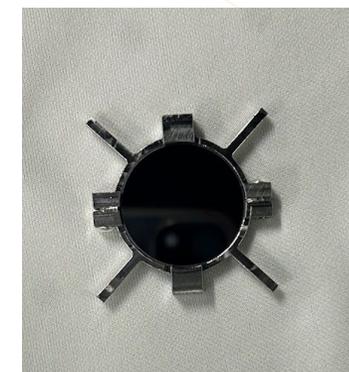
*Mirrors, currently uncoated*

# Methods



*8 Adjustment screws  
+4 in front*

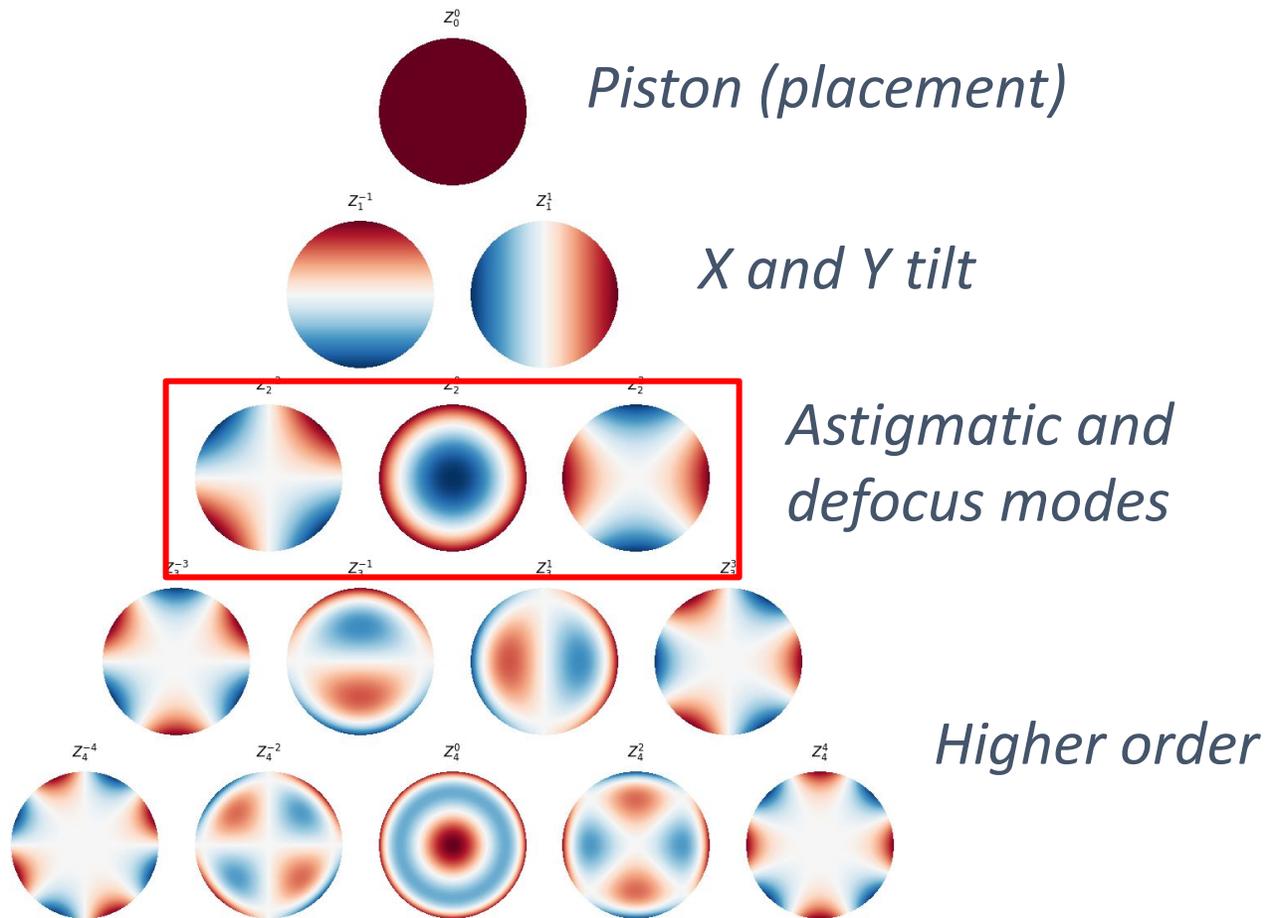
*Silicon mirror*



*Half ring*

*End Mirror Mount*

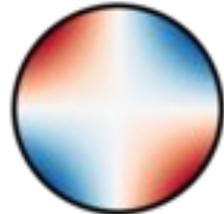
# Lensing into higher order modes



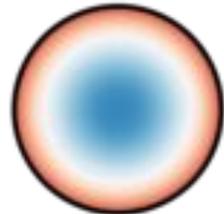
*Zernike Polynomials, orthogonal spherical special functions*

- Mirror is physically curved into higher order modes by screws
- Modes above are loss (contribute to contrast defects)
- Modes below can be 'zeroed' by placement of the mirror

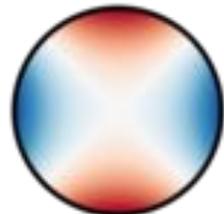
# Lensing into higher order modes



*Oblique astigmatism  
(order 3)*



*Defocus mode  
(order 4)*



*Vertical astigmatism  
(order 5)*

*Zernike  
Polynomials,  
orthogonal  
spherical special  
functions*

# Wavefront Measurement Methods

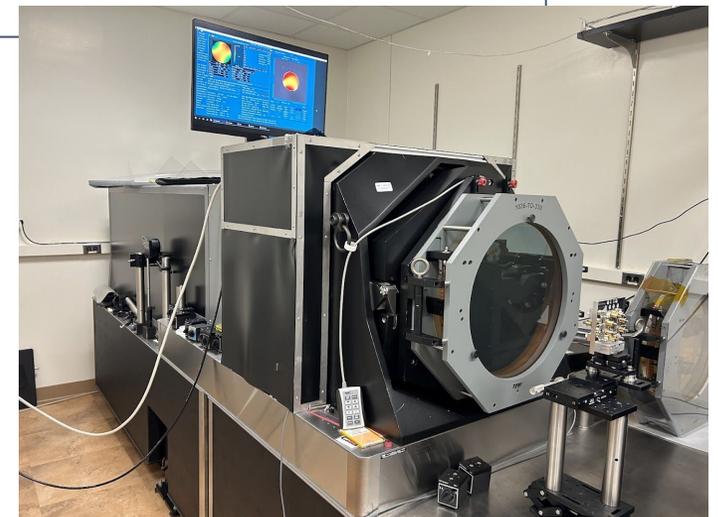
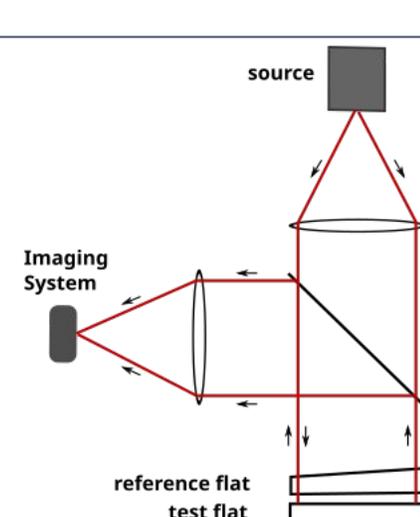
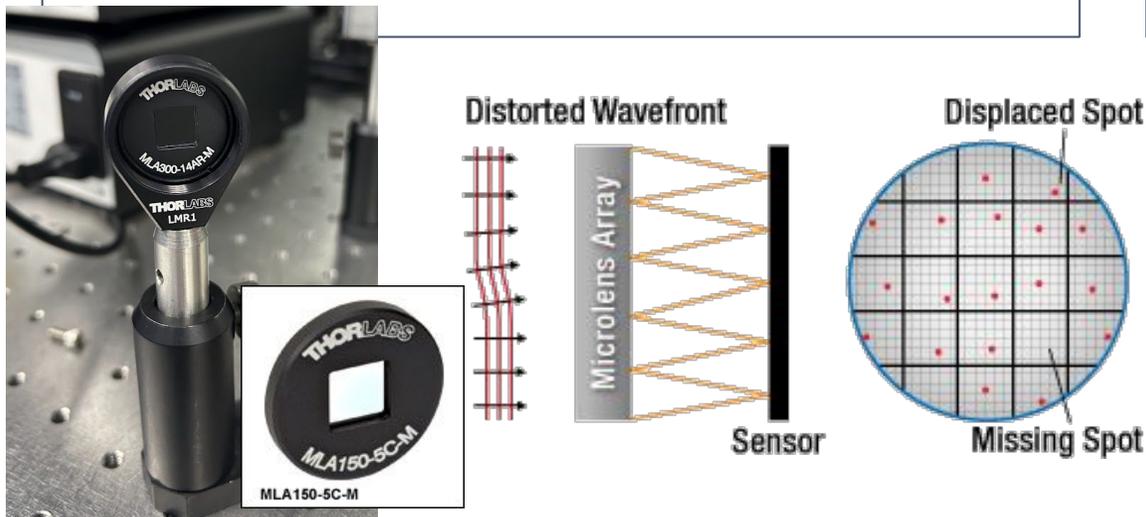


## Shack-Hartmann Wavefront Sensor:

- Less accurate of the two
- Uses a differential measurement from an array of powerful microlenses to reconstruct the wavefront

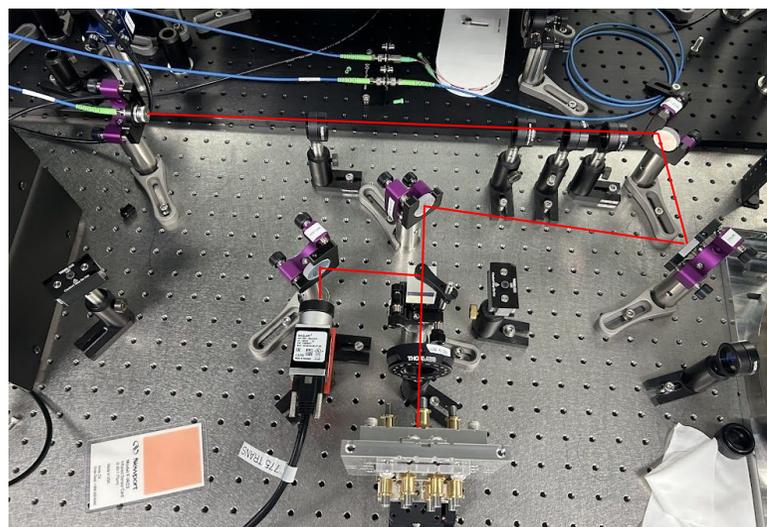
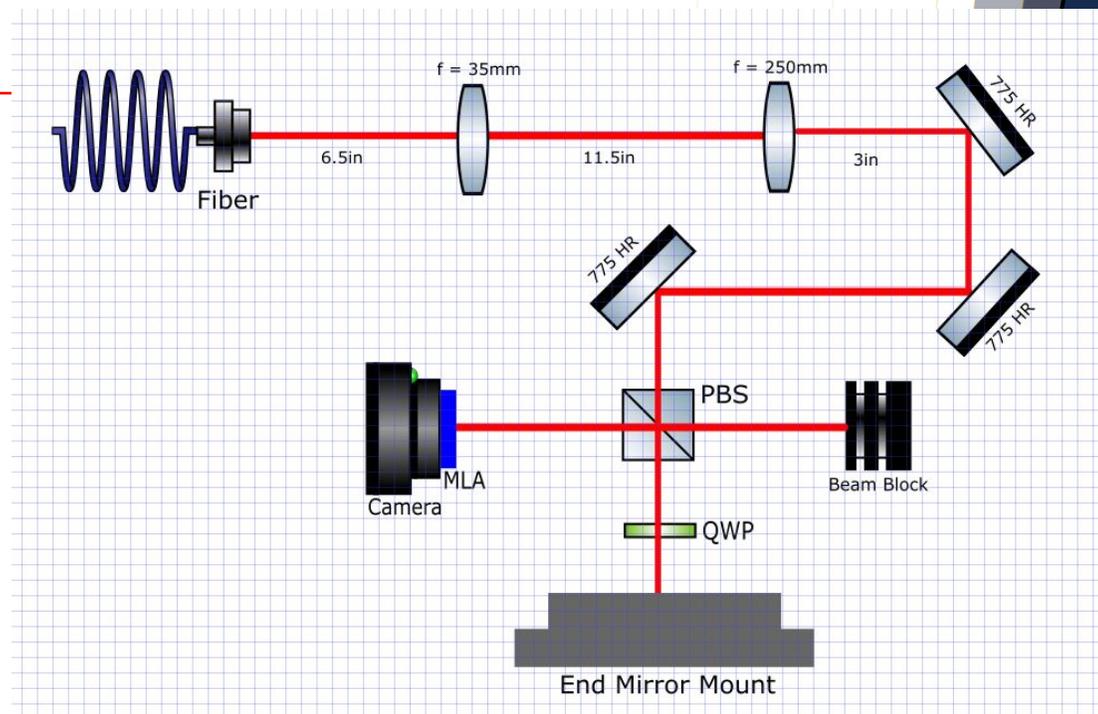
## Fizeau Interferometer:

- More accurate, used for LIGO Test Masses
- Measures difference in interference fringes between reference and test flat to reconstruct wavefront



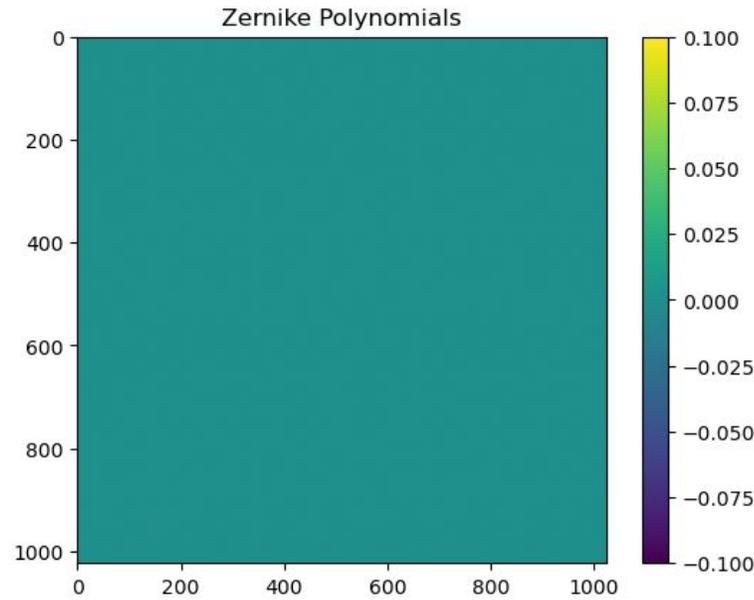
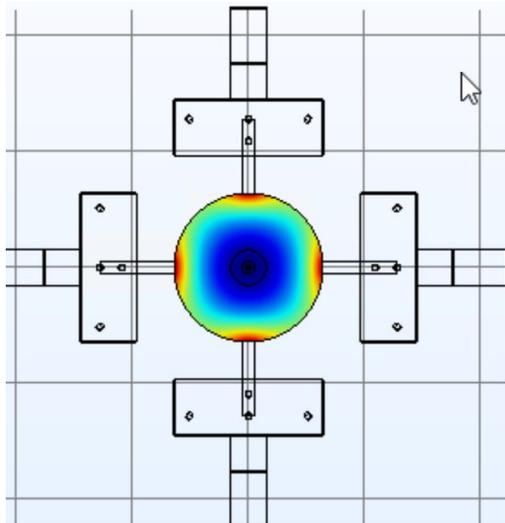
# Methods

- Imaged mirror without mount with the Fizeau
- Developed a pipeline for analyzing wavefront data, and using it to determine radius of curvature and displacement of the mirror
- Designed and built a setup for using the Shack-Hartmann Wavefront Sensor, took data with different modes
- Imaged different modes with the Fizeau interferometer



*Setup design for Shack-Hartmann Sensor*

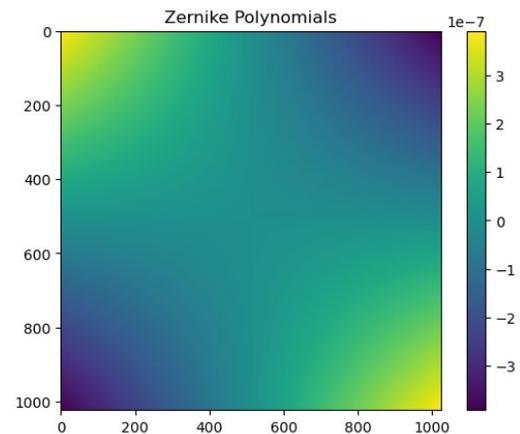
# Simulation



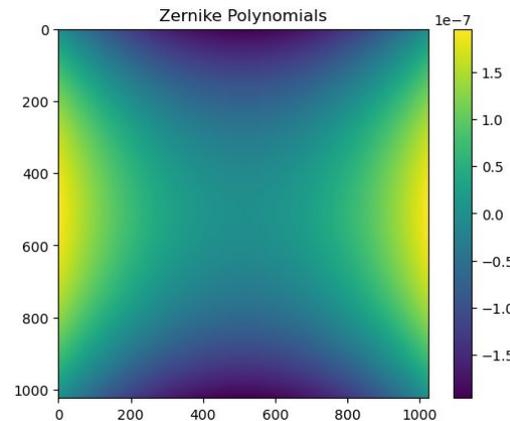
*COMSOL  
simulation of  
adding  
pressure to a  
mirror*

Mode	Coupling	Radius (D)
HG00	0.99997	4.75E-15
HG01	1.86E-17	-
HG10	1.39E-17	-
HG02	1.97E-16	1.29E-17
HG11	5.63E-19	4.37E-20
HG20	1.66E-16	1.53E-17

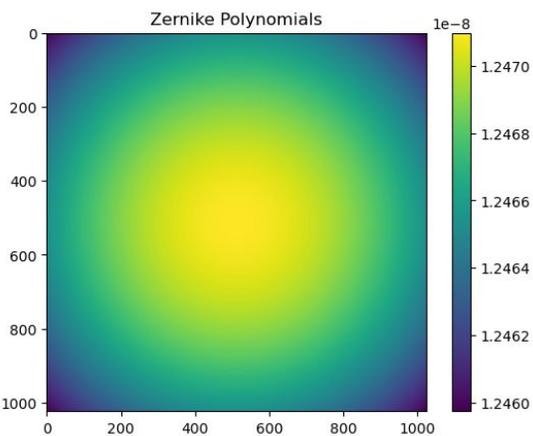
# Simulation



Mode	Coupling	Radius (D)
HG00	0.99949541	5.54E-05
HG01	2.63E-17	-
HG10	1.37E-17	-
HG02	0.00071305	5.53E-05
HG11	0.03173144	2.46E-03
HG20	0.00071305	5.53E-05



Mode	Coupling	Radius (D)
HG00	0.9994954	5.54E-05
HG01	1.15E-16	-
HG10	1.37E-17	-
HG02	0.022448	1.74E-03
HG11	1.37E-18	1.06E-19
HG20	0.022448	1.74E-03

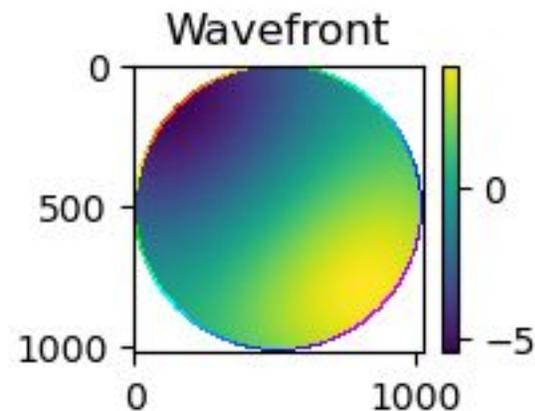
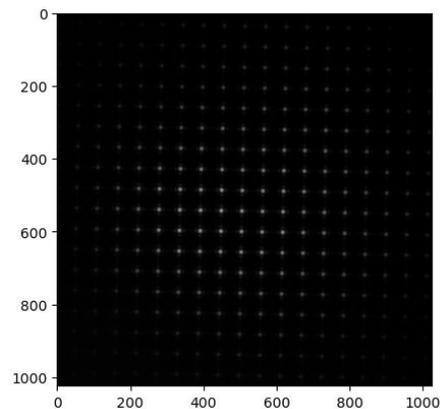


Mode	Coupling	Radius (D)
HG00	0.99999999	5.02E-14
HG01	2.81E-17	-
HG10	1.05E-17	-
HG02	6.43E-07	4.99E-08
HG11	2.80E-18	2.17E-19
HG20	6.43E-07	4.99E-08

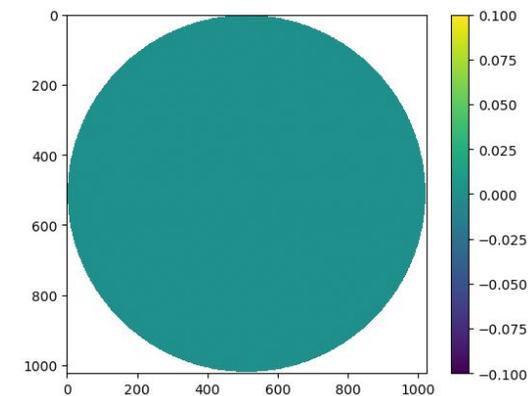
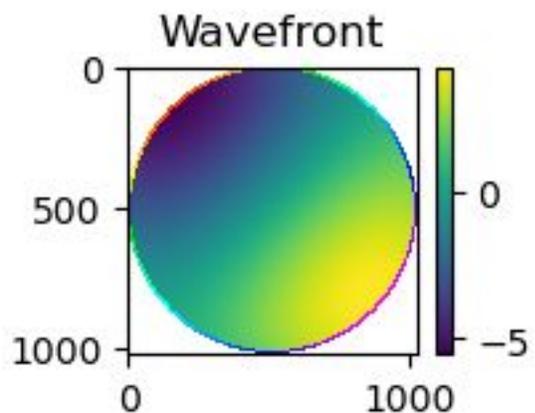
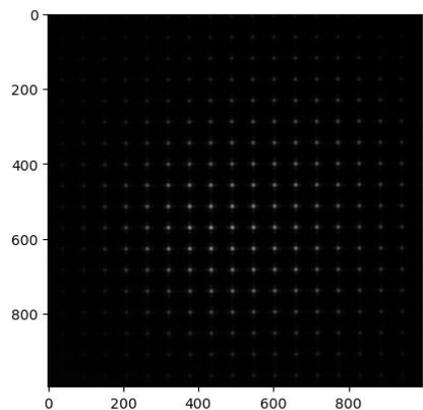
# Shack-Hartmann Sensor



*Flat wavefront*



*Curved wavefront*



*Subtracted wavefronts*

*Data from microlens array*

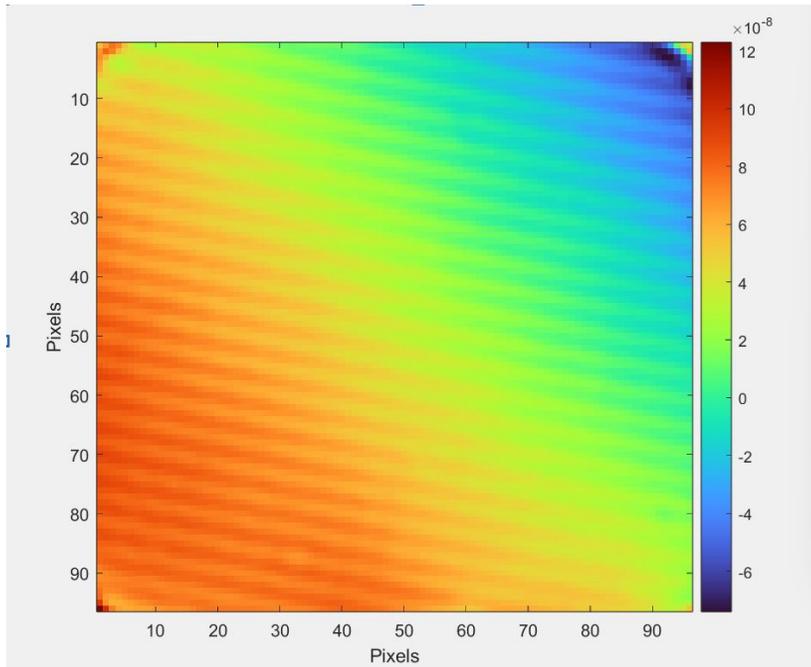
*Reconstructed wavefront*

**Shack - Hartmann**

# Fizeau: Flat mirror

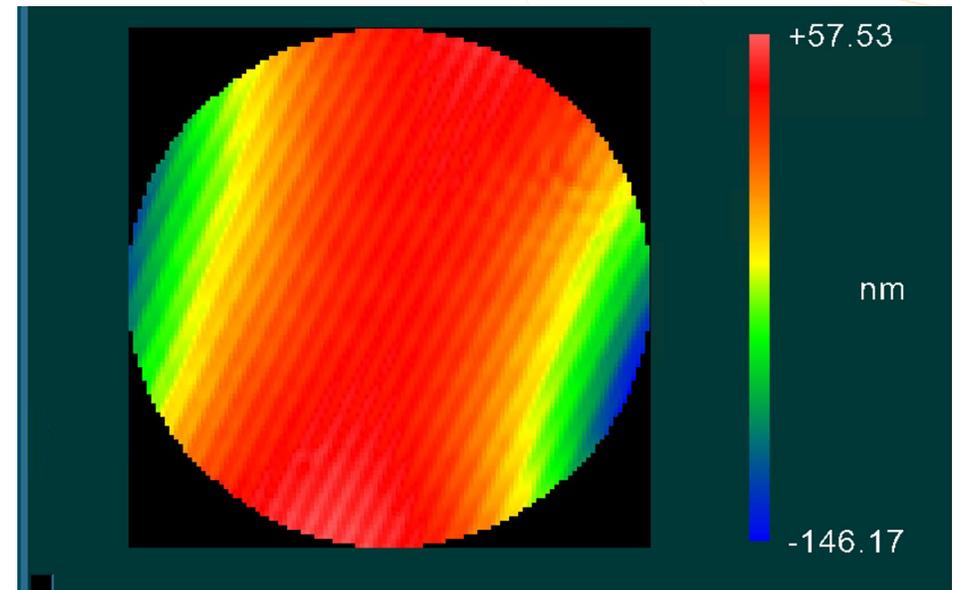


*Mirror outside of mount*



Coupling	0.999349524
Radius (D)	7.13878698e-05

*Mirror inside mount*



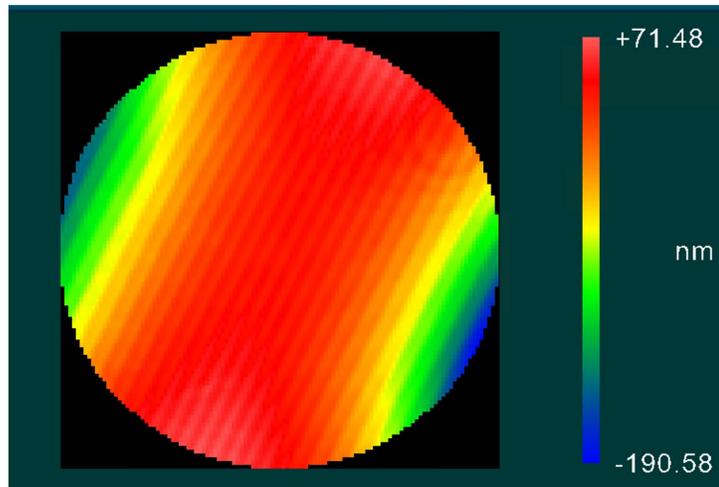
Coupling	0.999553816
Radius (D)	4.895232743e-05

# Fizeau continued: curved mirrors

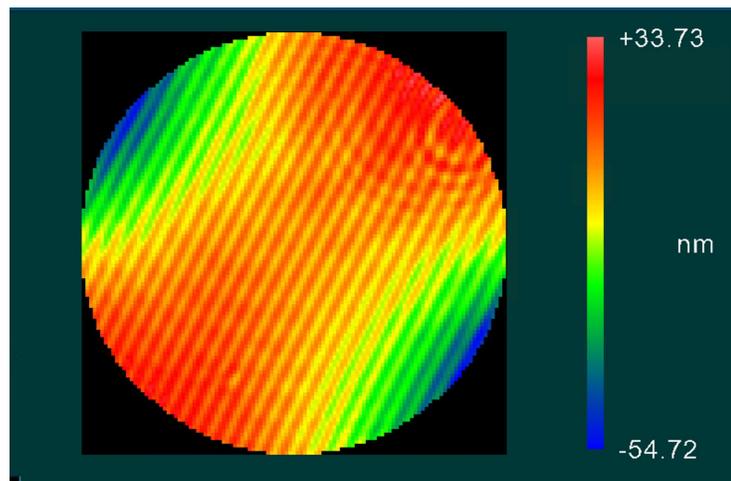


Oblique astigmatic mode ('+ shape')

*Wavefront image*



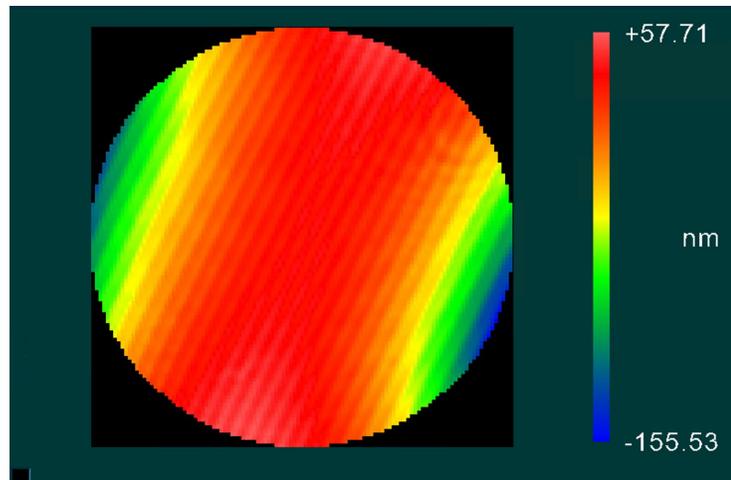
*Net change from unstressed mirror*



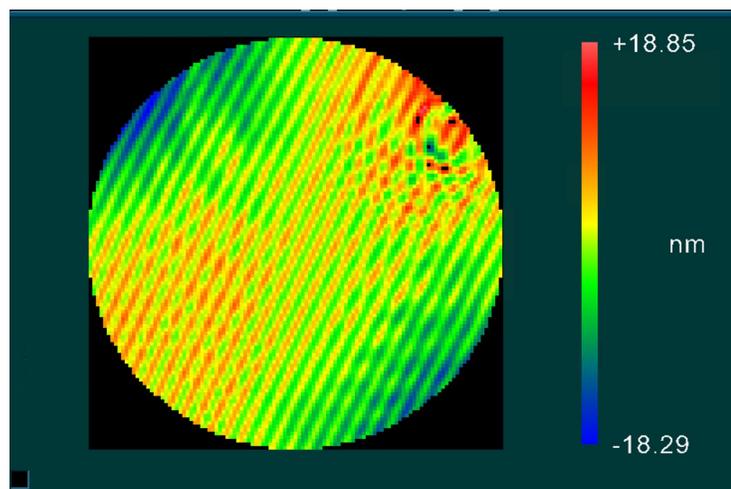
Plus Mode	Coefficient Simulated	Actual	Radius (D) Simulated	Actual
HG00	0.9994954	0.9999701	5.54E-05	3.27E-06
HG01	2.63E-17	1.20E-05	-	-
HG10	1.37E-17	1.02E-04	-	-
HG02	0.00071305	0.000123028	5.53E-05	1.59E-05
HG11	0.0317314	0.0010359	2.46E-03	8.03E-05
HG20	0.0007130	0.0002057	5.53E-05	9.54E-06

# Fizeau continued: curved mirrors

Defocus mode ('o shape')



*Wavefront image*



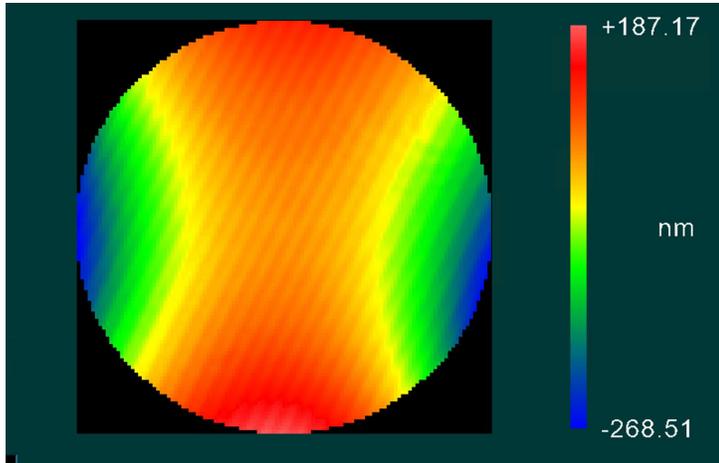
*Net change from unstressed mirror*

o mode	Coefficient		Radius (D)	
	Simulated	Actual	Simulated	Actual
HG00	0.999999	0.999928	5.02E-14	7.85E-06
HG01	2.81E-17	7.83E-05	-	-
HG10	1.05E-17	3.28E-05	-	-
HG02	6.43E-07	5.36E-04	4.99E-08	3.07E-05
HG11	2.80E-18	1.42E-04	2.17E-19	1.10E-05
HG20	6.43E-07	3.96E-04	4.99E-08	4.15E-05

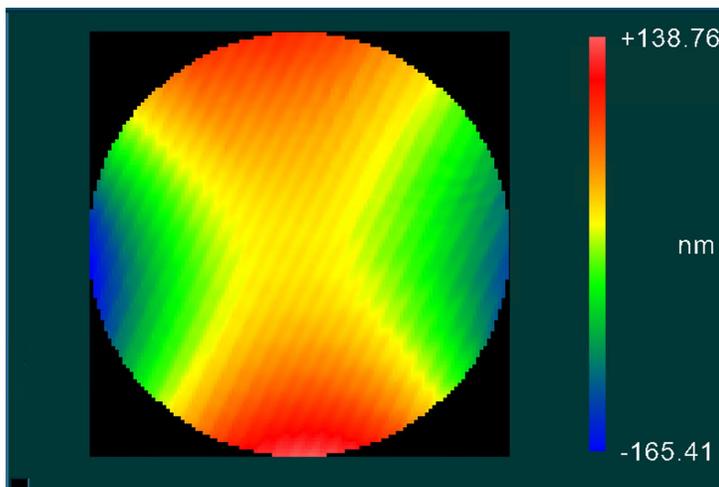
# Fizeau continued: curved mirrors



Vertical astigmatic mode ('x shape')



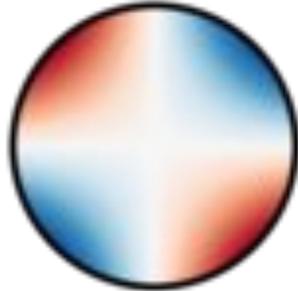
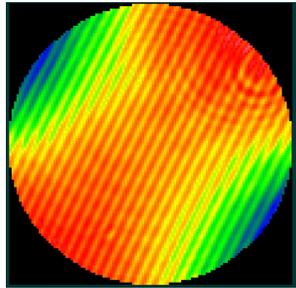
*Wavefront image*



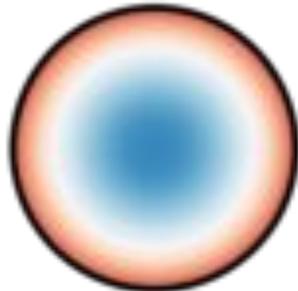
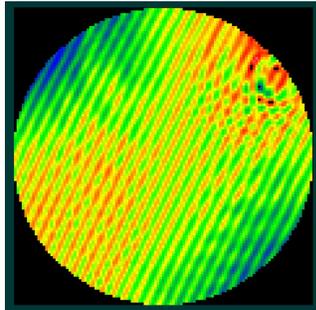
*Net change from unstressed mirror*

x	Coefficient		Radius (D)	
mode	Simulated	Actual	Simulated	Actual
HG00	0.9994954	0.9999837	5.54E-05	1.78E-06
HG01	1.15E-16	7.60E-05	-	-
HG10	1.37E-17	6.20E-05	-	-
HG02	0.0224488	0.0021739	1.74E-03	2.23E-04
HG11	1.37E-18	3.44E-04	1.06E-19	2.67E-05
HG20	0.0224488	0.0028726	1.74E-03	1.69E-04

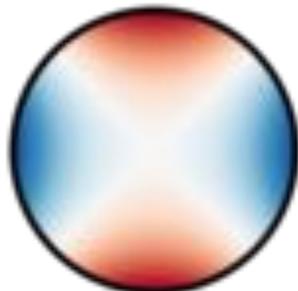
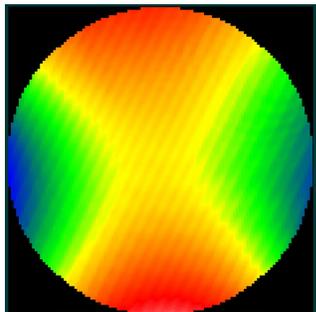
# Fizeau continued: curved mirrors



*Oblique astigmatism  
(order 3)*



*Defocus mode  
(order 4)*



*Vertical astigmatism  
(order 5)*

# Application to GQuEST: Loss



	Simulated	Fizeau	Loss (ppm)
Flat mirror	8.66E-14	5.17E-05	51.7
Plus	1.02E-06	2.51E-05	25.1
O	8.82E-14	4.11E-05	41.1
X	1.02E-06	5.11E-05	51.1

- Loss is a measure of how many photons are scattered into higher order modes
- GQuEST has a loss budget on the order of  $\sim 100$  ppm at most for mirrors
- Important to make sure mirrors are not a major contributor to this overall loss

# Conclusions



- We can properly lens into the astigmatic modes, but have difficulty doing so into the defocus mode
- The Shack-Hartmann Sensor, while helpful, is not precise enough to measure changes in modes
- The modes produced by the end mirror mount generally matches the COMSOL and python simulations
- Positive first step towards making mirrors that match in modes

# Next Steps



- Implement a different data analysis process for the Shack-Hartmann sensor to potentially improve its ability to reconstruct wavefronts
- Continue to use and improve the pipeline for analyzing data
- Continue trying to lens into the defocus mode
- Reducing loss into higher order modes
- Replacing these mirrors in the half ring with spokes and mirrors as one piece
- Coating the mirrors

# Questions?



## *Acknowledgements:*

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# Extra Info and Slides

# How did we make the Shack-Hartmann wavefront?



$$\Phi(x, y) = \sum_{i=1}^I a_i Z_i(x, y) \quad \longrightarrow \quad \begin{aligned} \frac{\partial \Phi}{\partial x} &= \sum_{i=1}^I a_i \frac{\partial Z_i(x, y)}{\partial x} \\ \frac{\partial \Phi}{\partial y} &= \sum_{i=1}^I a_i \frac{\partial Z_i(x, y)}{\partial y} \end{aligned}$$

$P = (\text{x shift 1, x shift 2, .... x shift } k, \text{ y shift 1, y shift 2....y shift } k)$

$$D = \begin{pmatrix} \frac{\partial Z_2(x,y)_1}{\partial x} & \frac{\partial Z_2(x,y)_2}{\partial x} & \dots & \frac{\partial Z_2(x,y)_1}{\partial y} & \dots & \frac{\partial Z_2(x,y)_k}{\partial y} \\ \dots & \dots & \dots & \dots & \dots & \dots \\ \frac{\partial Z_i(x,y)_1}{\partial x} & \frac{\partial Z_i(x,y)_2}{\partial x} & \dots & \frac{\partial Z_i(x,y)_1}{\partial y} & \dots & \frac{\partial Z_i(x,y)_k}{\partial y} \end{pmatrix}$$

$$P = D^t A$$

$$DP = DD^t A$$

$$A = (DD^t)^{-1} DP$$

$$A = (a_1, a_2, a_3 \dots a_i)$$

# How does coupling relate to radius of curvature?



$$u_n(x, z) = \left(\frac{2}{\pi}\right)^{1/4} \left(\frac{1}{2^n n! w_0}\right) \left(\frac{q_0}{q(z)}\right)^{1/2} \left(\frac{q_0 q^*(z)}{q_0^* q(z)}\right)^{n/2} H_n \left(\frac{\sqrt{2}x}{w(z)}\right) \exp\left(-i\frac{kx^2}{2q(z)}\right)$$

$$k_{mn}(D, q_1, q_2) = \int u_n^*(x, q_1) e^{i\frac{kDx^2}{2}} u_m(x, q_2) dx$$

$$k_{00} = \left(1 - \frac{i}{4} Dkw^2\right)^{-1/2}$$

$$D = \frac{-4i}{kw^2} \left(1 - \frac{1}{k_{00}^2}\right)$$

$$k_{02} = \frac{1}{\sqrt{2}} \frac{\frac{1}{4} Dkw^2}{\left(1 - \frac{i}{4} Dkw^2\right)^{3/2}}$$

$$D \approx \frac{4\sqrt{2}k_{02}}{kw^2}$$

# What are Zernike Polynomials?



$$Z_n^m(\rho, \phi) = R_n^m(\rho) \cos(m\phi)$$

$$W(\rho, \phi) = \sum_{n,m} a_{nm} Z_n^m(\rho, \phi)$$

$$Z_n^{-m}(\rho, \phi) = R_n^m(\rho) \sin(m\phi)$$

$$j = \frac{n(n+1) + m}{2}$$

$$R_n^m(\rho) = \sum_{k=0}^{\frac{n-m}{2}} \frac{(-1)^k (n-k)!}{k! \left(\frac{n+1}{2} - k\right)! \left(\frac{n-m}{2} - k\right)!} \rho^{n-2k}$$

# What do the adjustment screws do?

